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Improved Processes & Parameterisation
for Prediction in Cold Regions

Evaluation of the heat-pulse probe method for measuring frozen soil moisture content

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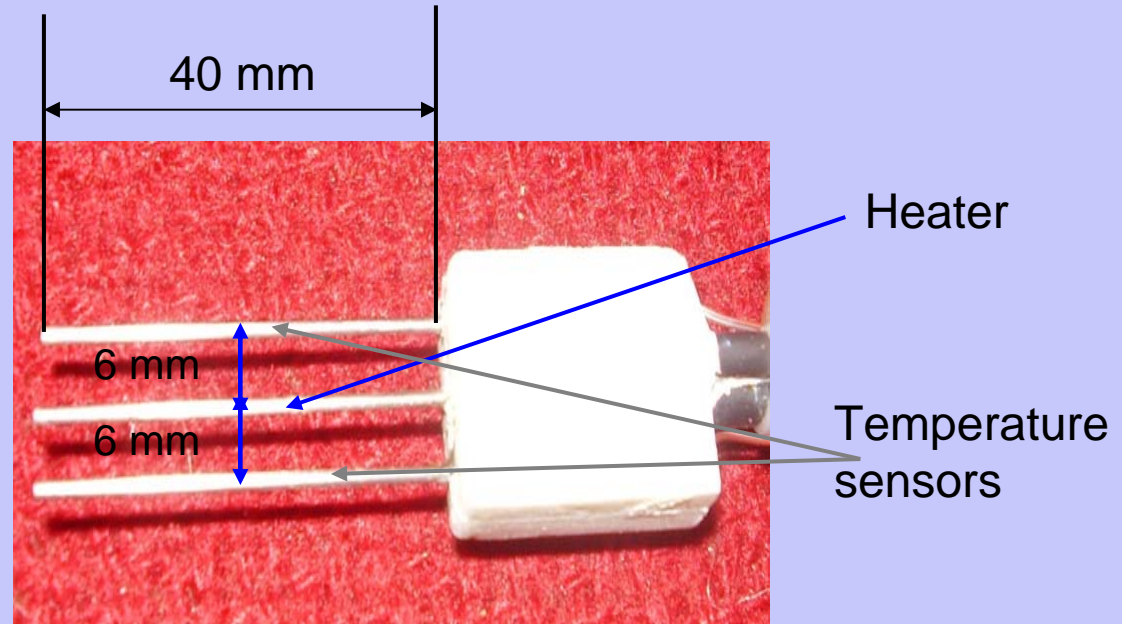
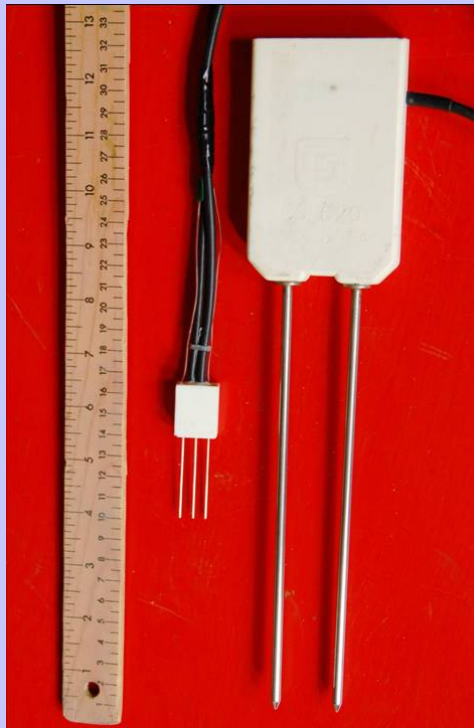
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What is Heat Pulse Probe (HPP)

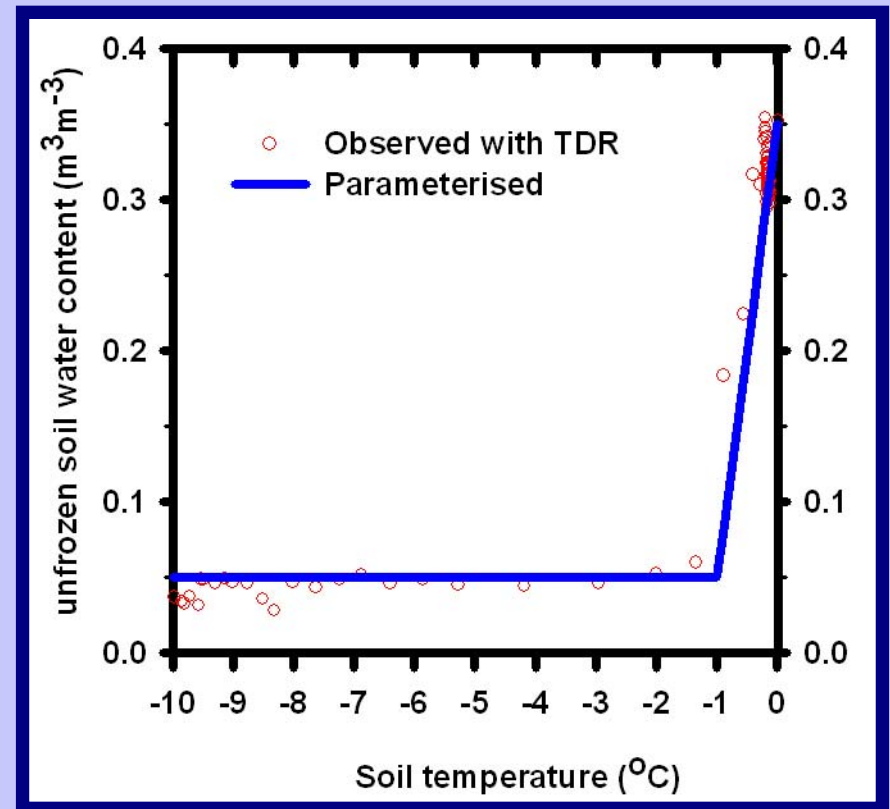


$$\Delta T = f(C, q, t_0, t, r) \quad \longrightarrow \quad \text{Determines } C$$

$$C = \Sigma (C_m \theta_m + C_o \theta_o + C_l \theta_l + C_i \theta_i) \quad \longrightarrow \quad \text{Determines } \theta_l, \theta_i$$

Why HPP for soil ice ?

- ▶ No other options for θ_i other than radioactive methods.
- ▶ Successfully tested in unfrozen soil.
- ▶ θ_i could be determined by TDR or θ_i-T curves.



HPP has the potential for soil ice measurements with:

- ✓ Relatively low cost
- ✓ Continuous measurements
- ✓ Minimum disturbance to natural conditions

How to make HPP work for frozen soil?

Problems for frozen soils:

Possible ice melting will null the assumptions of current mathematical solutions for HPP:

- ✓ All energy is used to raise soil temperature by conduction
- ✓ soil thermal properties (C , λ , κ) are constant and homogenous

Possible solutions:

- ✓ Control q , t_0 to limit melting
- ✓ Revise the mathematical solution to include soil thawing

Lab experiments

Material:
fine sand with porosity of 0.35

Tests conducted

| Controls | Ranges |
|----------|------------------------------|
| q | 100 – 2000 J m ⁻¹ |
| t_0 | 8s, 15s, 30s, 60s |
| T | 20 °C, -2 °C, -4°C, -10°C |
| s | 100%, 50%, 25%, 1% |



Mathematical solutions

1. Instantaneous Infinite Line Source (IILS)

$$\Delta T(r,t) = \frac{q}{4\pi\lambda t} \exp\left(\frac{-r^2}{4\kappa t}\right)$$

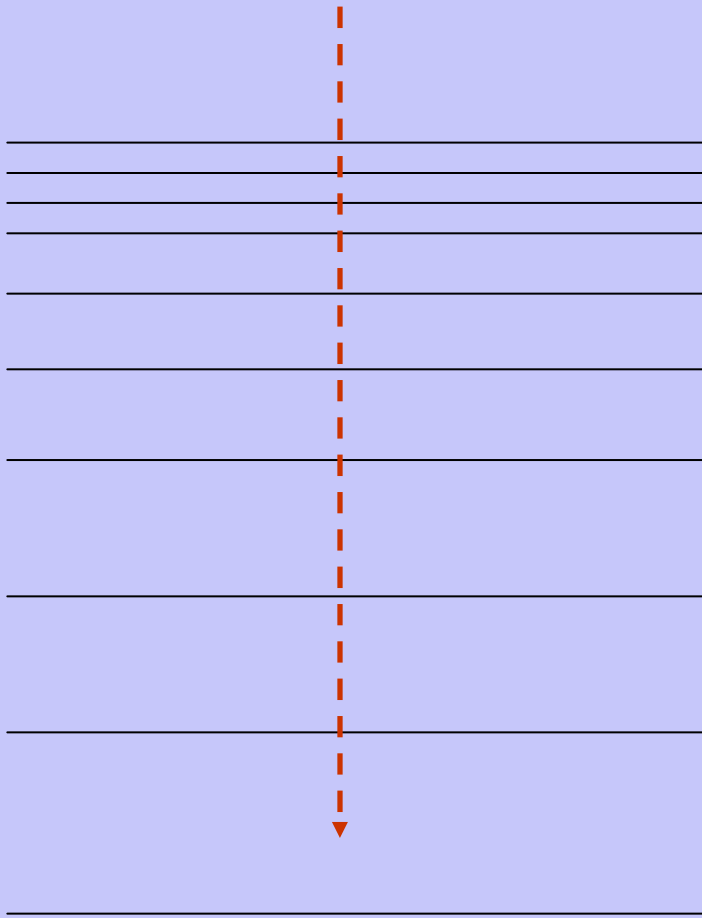
2. Pulsed Infinite Line Source (PILS)

$$\Delta T(r,t) = \begin{cases} \frac{-q'}{4\pi\lambda} Ei\left(\frac{-r^2}{4\kappa t}\right) & 0 < t \leq t_0 \\ \frac{q'}{4\pi\lambda} \left\{ Ei\left[\frac{-r^2}{4\kappa(t-t_0)}\right] - Ei\left(\frac{-r^2}{4\kappa t}\right) \right\} & t > t_0 \end{cases}$$

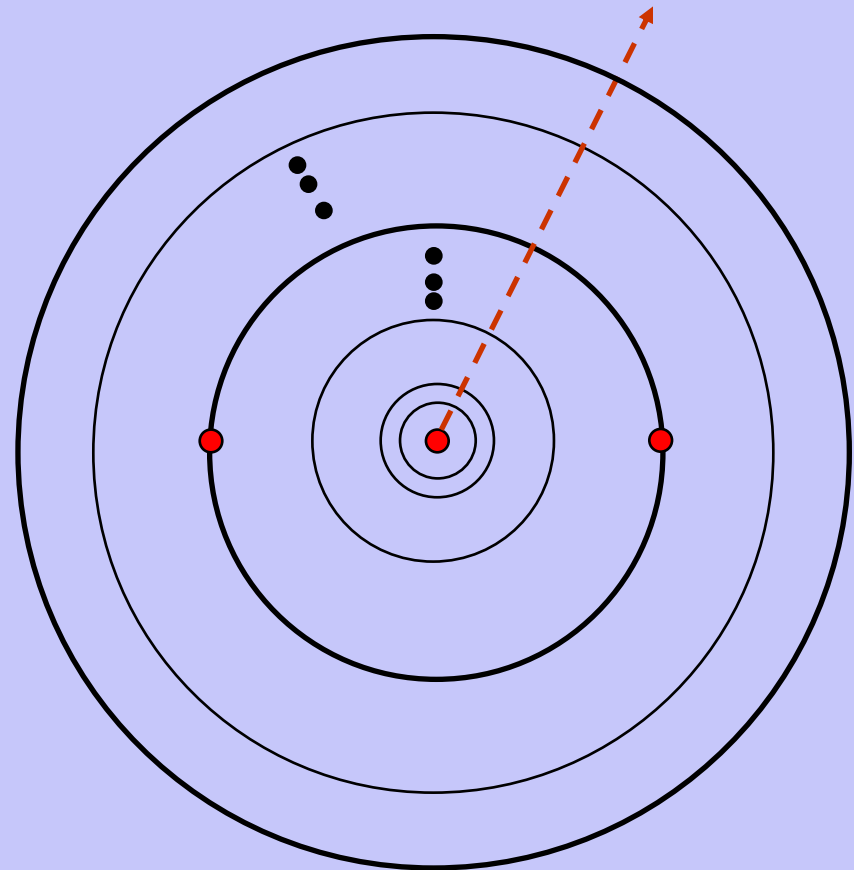
3. Finite Difference Numerical Model (FDNM)

$$C_p \frac{\partial T}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} \left(rK \frac{\partial T}{\partial r} \right) + q' \qquad C_p = C_v + \rho_i L \frac{d\theta_u}{dT}$$

The Numerical Scheme



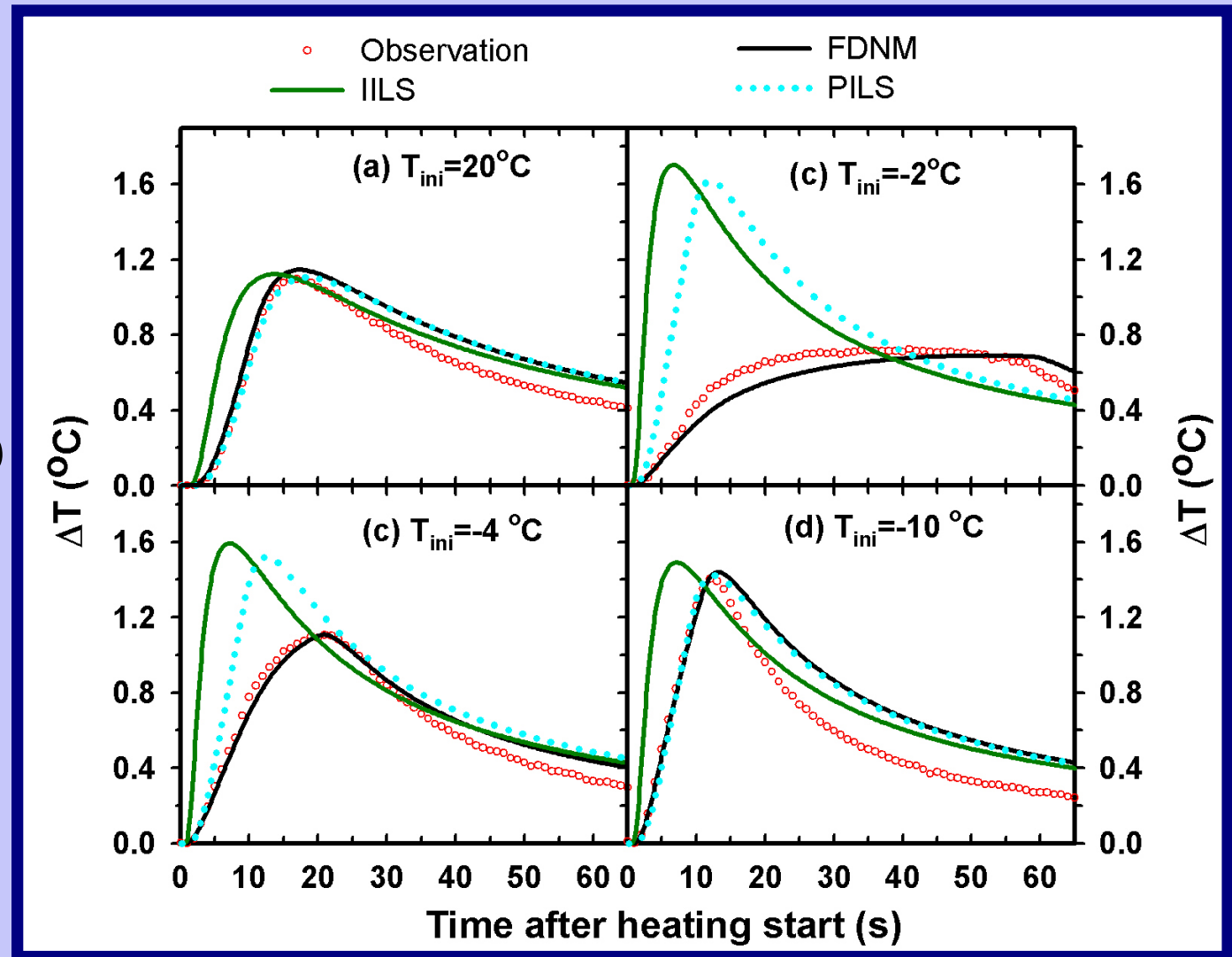
Vertical system



Radial system

Performance of three methods in different initial temperature

$q \approx 900 \text{ J m}^{-1}$
 $t_0 = 8 \text{ seconds}$
 $s = 1.0 \text{ (Saturated)}$

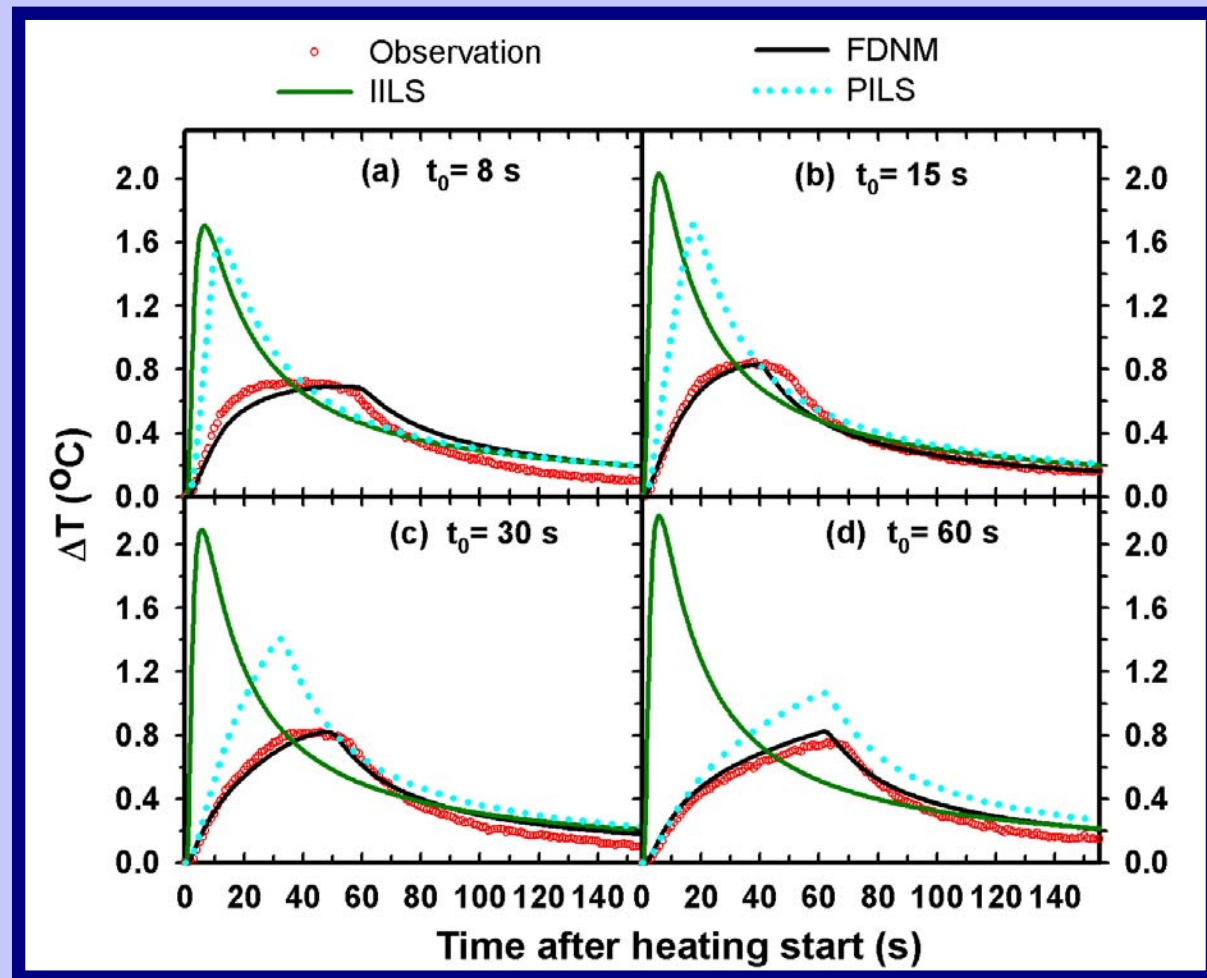


Performance of three methods under different heating time

$$q \approx 1000 \text{ J m}^{-1}$$

$$T_{\text{ini}} \approx -2.0 \text{ }^{\circ}\text{C}$$

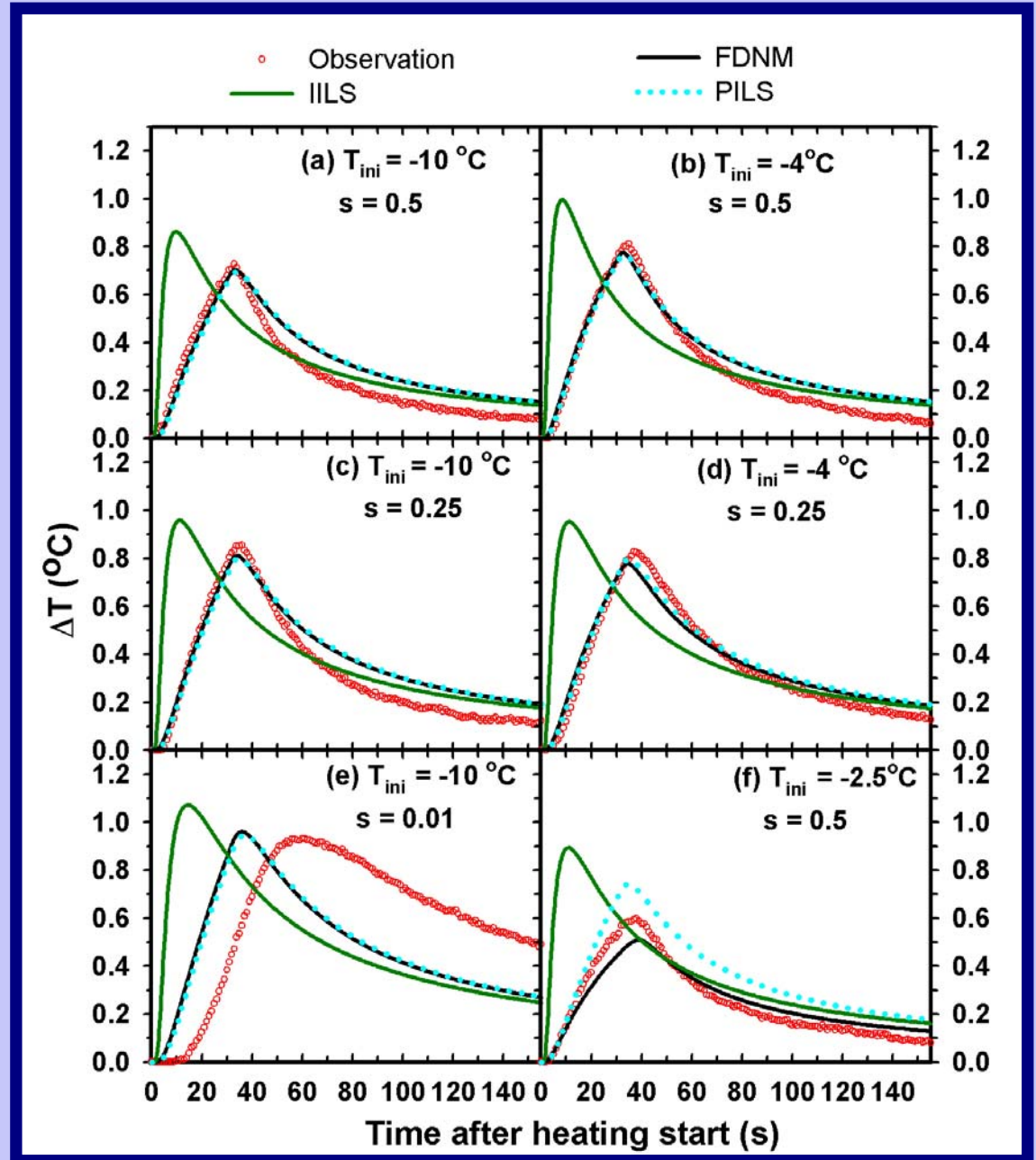
$$s = 1.0 \text{ (saturated)}$$



Performance of three methods under different moisture and temperature combinations

$$q \approx 450 \text{ J m}^{-1}$$

$$t_0 = 30 \text{ seconds}$$

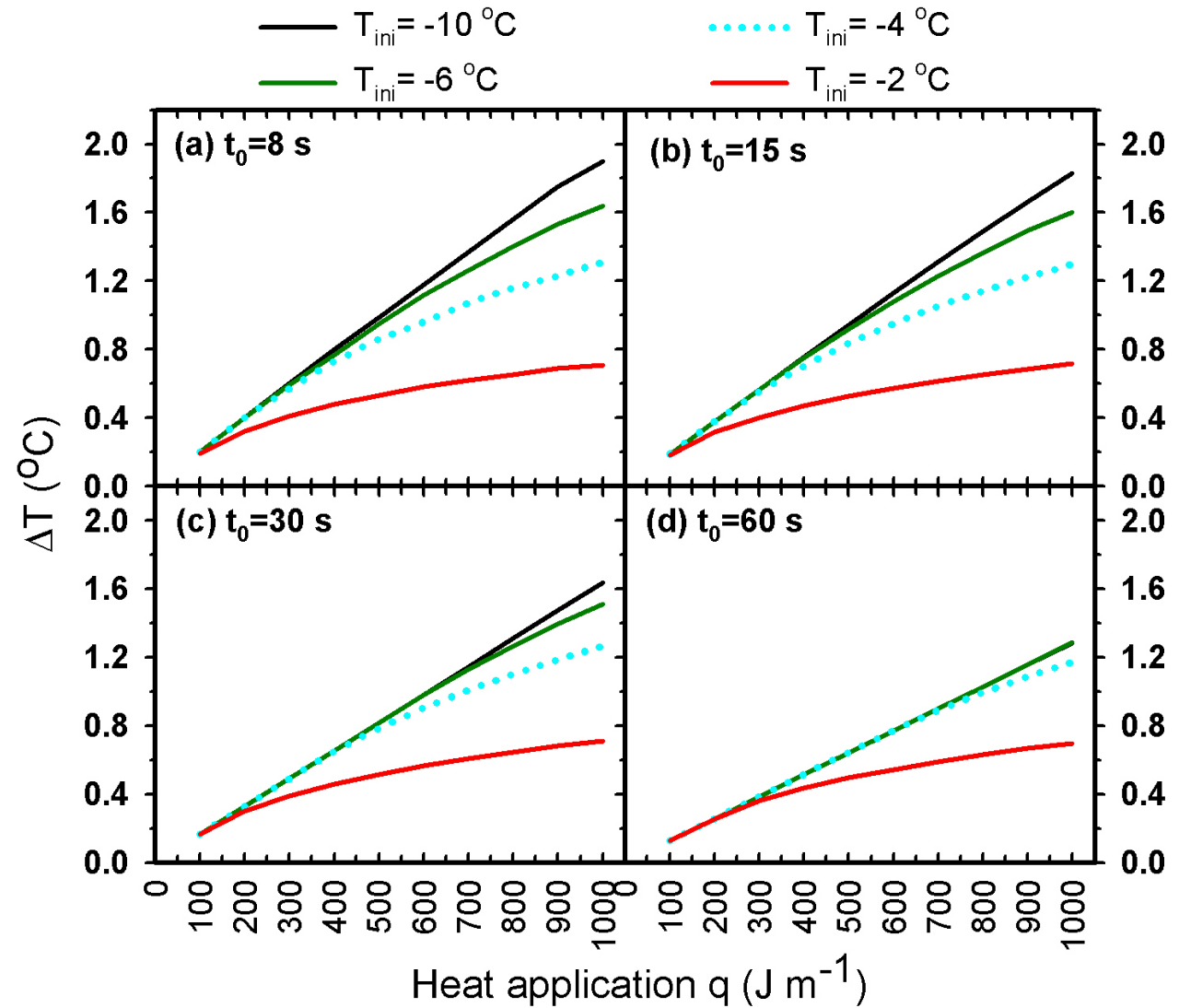


Sensitivity of ΔT to heat application

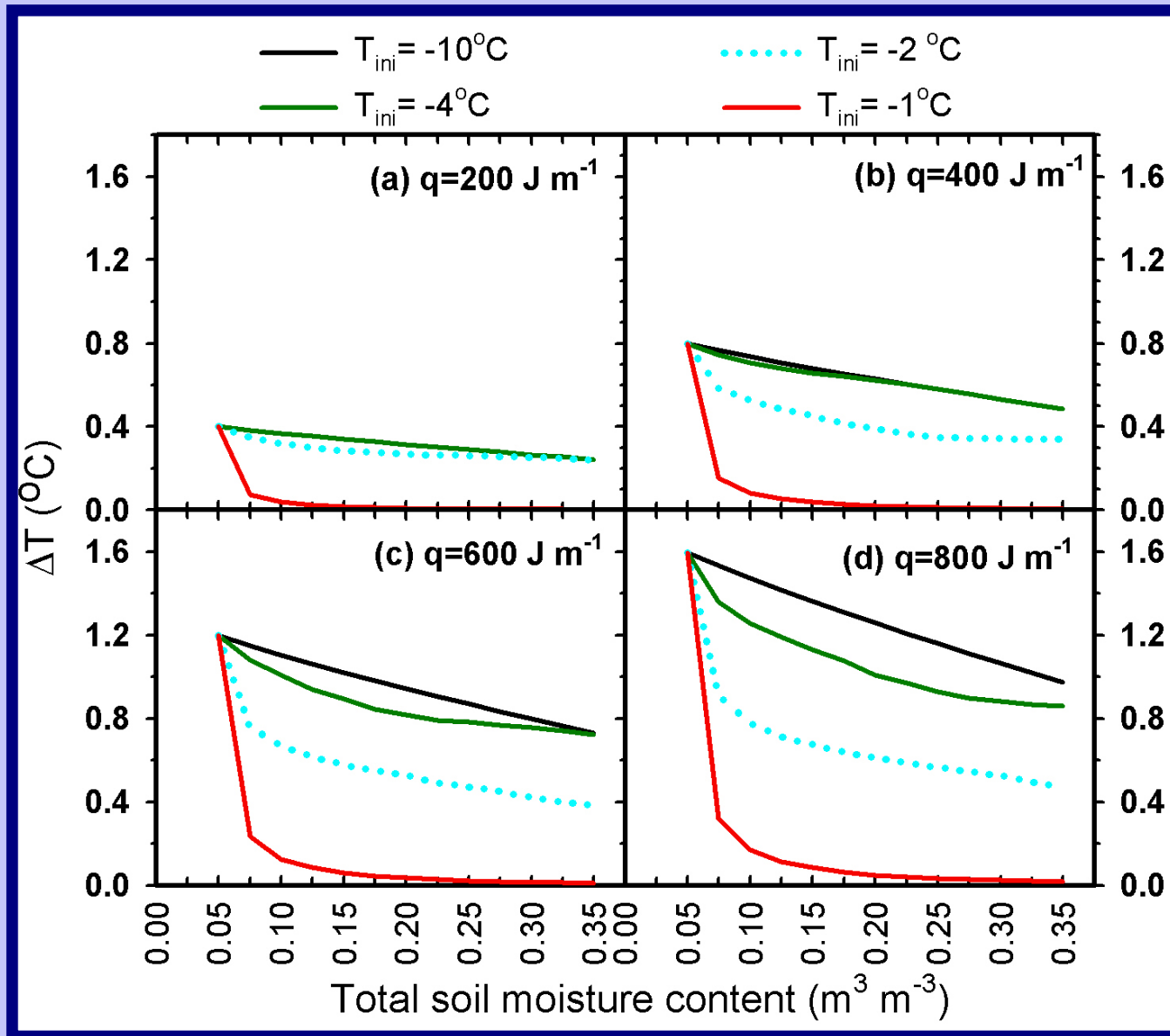
$$q = 100 \sim 1000 \text{ J m}^{-1}$$

$$T_{\text{ini}} = -2 \sim -10 \text{ }^{\circ}\text{C}$$

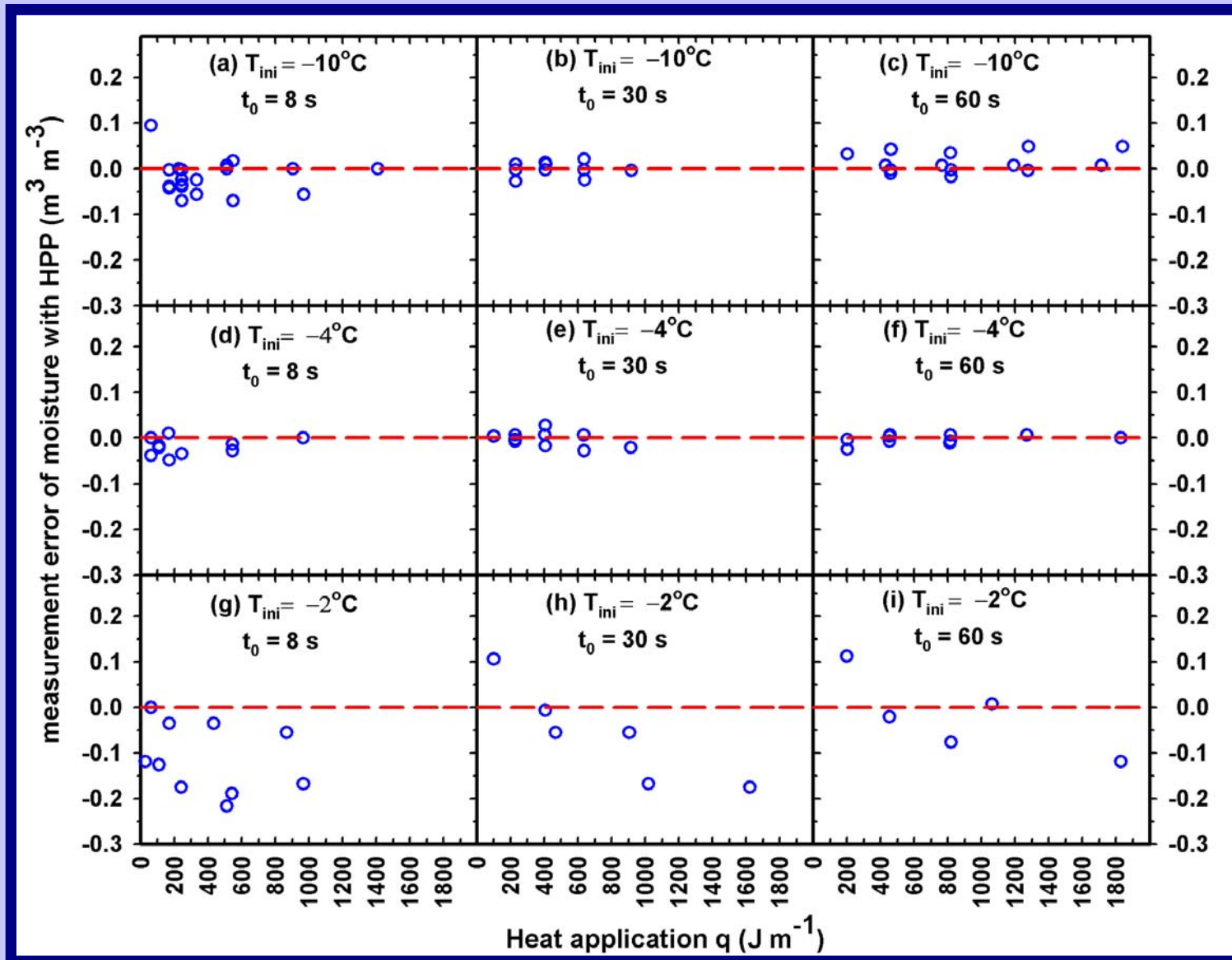
$$s = 0.5$$



Sensitivity of ΔT to total moisture content (θ) under different heat applications (HPP applicability)



Error distribution of frozen moisture measurement of HPP with calibrated probe spacing (5.0-6.2mm)



Conclusions

- ◆ Only the numerical model could represent the measured ΔT curves once ice melting occurs during HPP measurements.
- ◆ Below -4°C , ice melting could be controlled to a limited level such that it has little effects to HPP measurements .
- ◆ The measurement errors of θ were well within $\pm 0.05 \text{ m}^3 \text{ m}^{-3}$ under -4°C , but become unpredictable between -2°C and 0°C .
- ◆ The failure of HPP between -2°C and 0°C are mainly due to the retarded response of ΔT to changing θ and q .
- ◆ The probe spacing is a very sensitive parameter and needs recalibration each time the probe inserted into soil or the soil goes through a thawing/freezing processes.